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Title: Assessment of double shell ablator asymmetry sources and shape control

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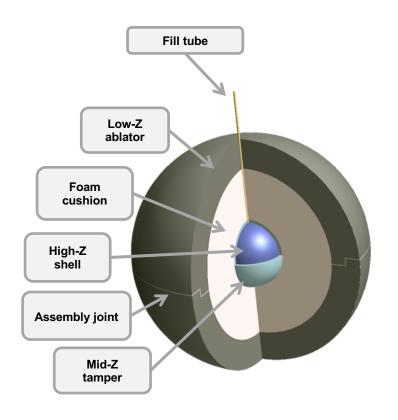
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Assessment of double shell ablator asymmetry sources and shape control

L2 Milestone Review

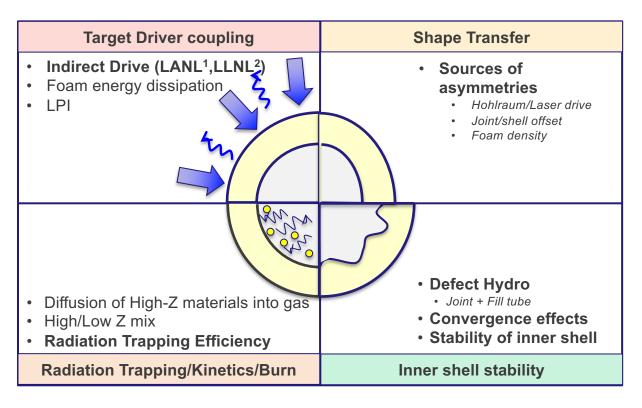


Ryan Sacks, Eric Loomis, Paul Keiter, Harry Robey for LANL double shell team

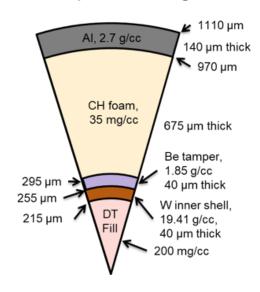
July 14, 2021



We have a work break-down framework for addressing key gaps in multi-shell physics



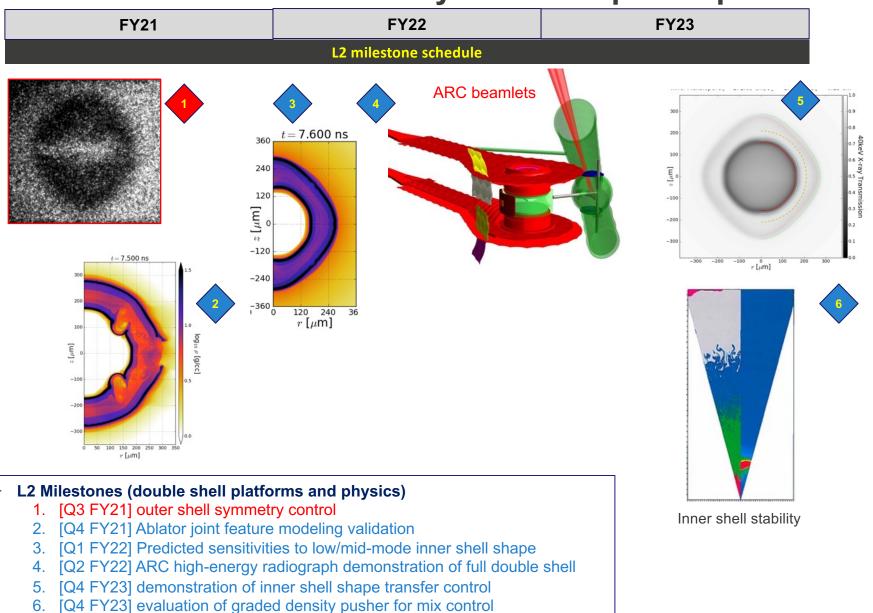
LANL point design



¹E. Merritt et al Physics of Plasmas **26**, 052702 (2019)

²Y. Ping et al., Nature Physics (2018)

An L2 milestone schedule was submitted to NNSA in 2020 based on our 5-year development plan



This L2 milestone definition and assessment approach

Definition:

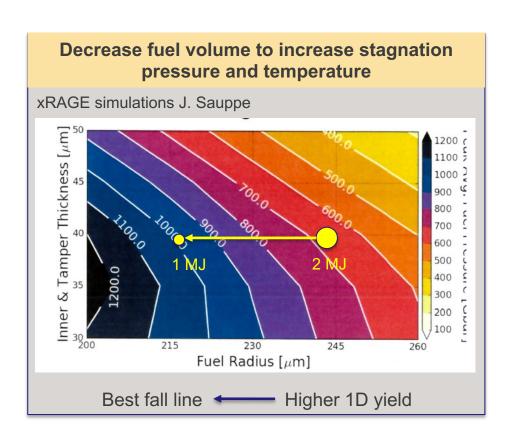
- Complete assessment of outer-shell shape asymmetry, including identification of sources and quantification of control.
 - Measurements of outer shell shape are evaluated and compared with known and suspected sources of asymmetry
 - Panel evaluation of the completeness of the analysis and identify unconsidered sources of asymmetry

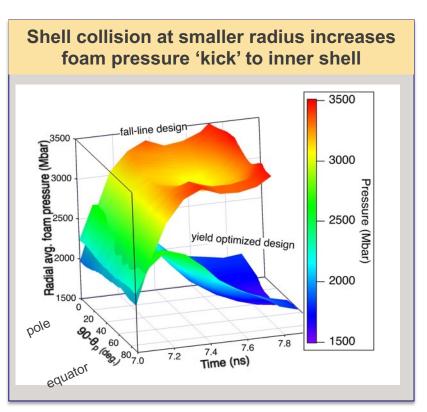
Approach:

- HYDRA integrated hohlraum/capsule simulation sensitivities to asymmetry sources (Loomis)
- Comparison of shape data to current best hohlraum model HYDRA postshots (Sacks, Keiter, Robey)



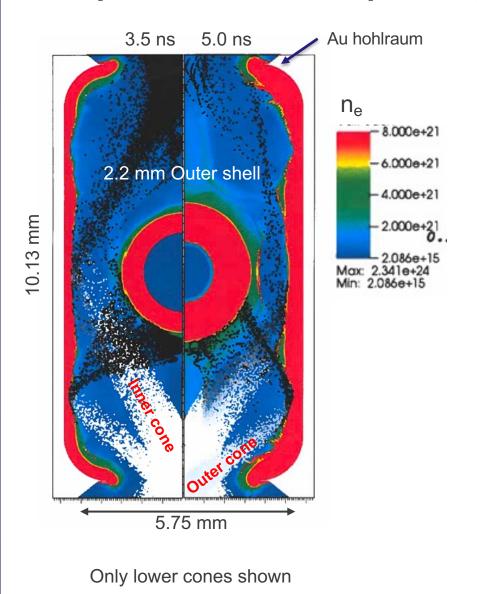
LANL point design double shell trades-off high 1D yield for robustness against asymmetries





High stagnation pressure and high, sustained collision foam pressure leads to 'upstream' burn, which reduces time for asymmetries to perturb fuel

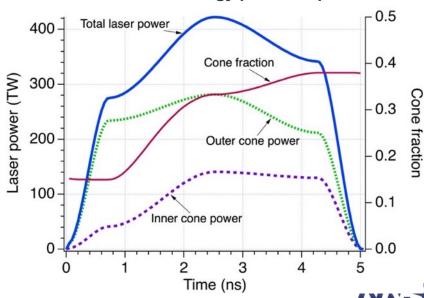
Hohlraum low-mode asymmetries mostly come from nonoptimal laser cone pointing and laser power balance



Hohlraum asymmetry sources

- Pulse shape (CF vs time)
- Beam pointing
- Hohlraum fill density
- Backscatter, glint and CBET
- Preheat (mainly inner shell)

1.5 MJ laser energy pulse shape



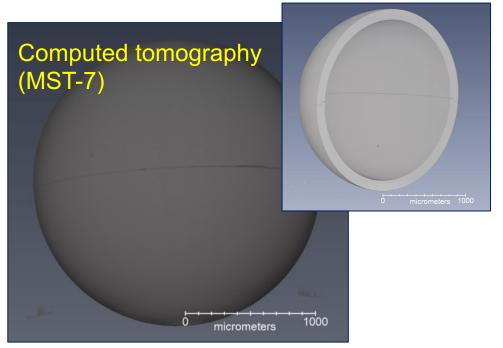
Capsule ablator asymmetries arise from thickness variations and non-closure/alignment of equatorial joint



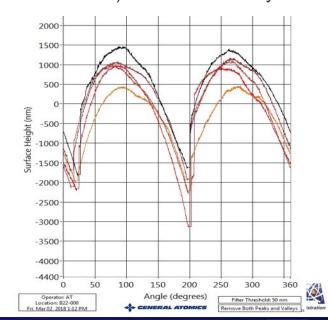
- Al hemi-shells are diamond turned to ~300 nm surface precision
- Registration of inner to outer surface can only be controlled to ~2 μm

Ablator asymmetry sources/sensitivities

- Hemi-shell outer/inner surface machining modes
- Hemi-shell surfaces nonconcentricity
- Hemi-shell assembly 3D offset (tied to joint feature)

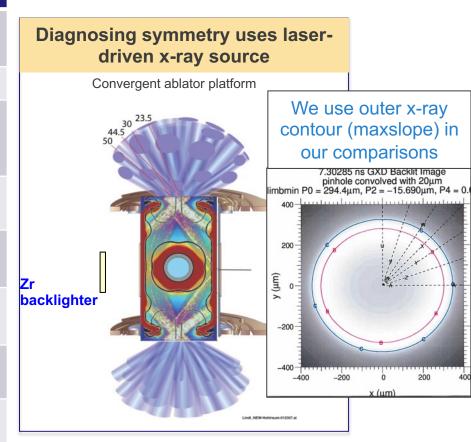


Atomic force microscopy (AFM, General Atomics) outer surface only



We use modern physics model standards in hohlraum simulations and x-ray backlighting to assess shape

HYDRA parameter	Sensitivity studies	Postshot simulations
Au wall zones	40 A first zone	same
DCA Au opac.	yes	yes
Photon group resolution (total bins)	120	85 (180 underway)
Laser rays per cone	600	same
Laser power multiplier	0.94	0.94
Non-local e- transport	Used	Flux limited (non-local underway)
Self consistent MHD	Not used	Not used
Inline CBET	Not yet used	Not yet used
Angular zoning (degrees/zone)	1	same

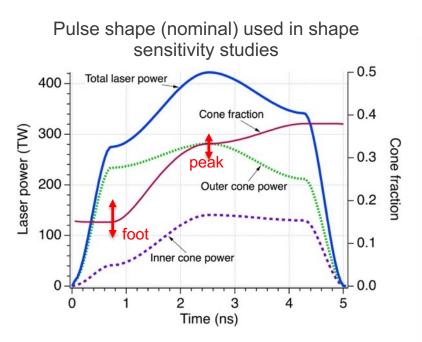


J.R. Rygg et al., Phys. Rev. Letts. 195001 (2014)

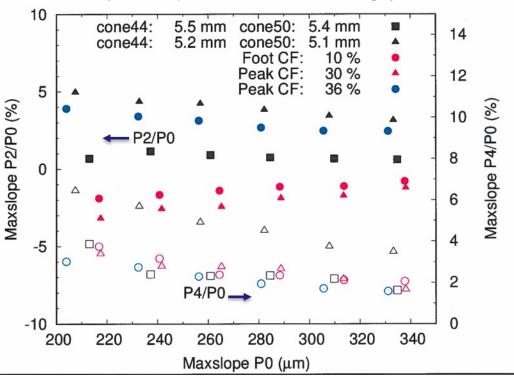




Hohlraum symmetry is controlled by time-dependent cone fraction and beam pointing

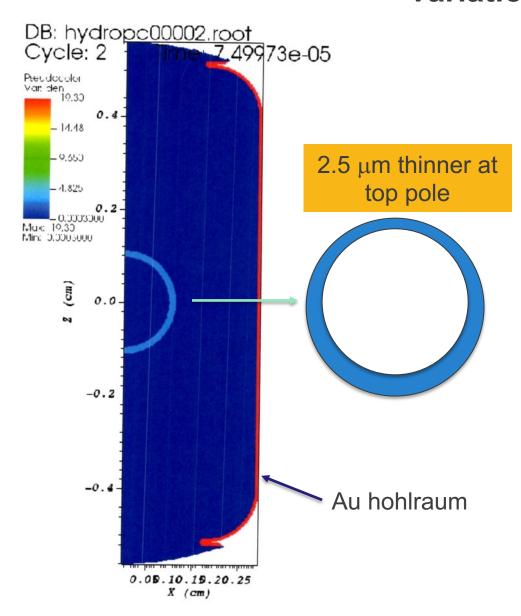


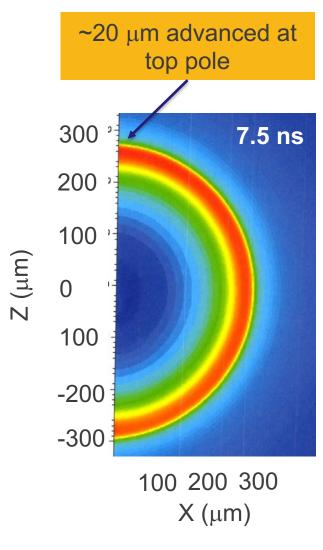
Predicted ablator P2 (closed) and P4 (open) Legendre amplitude trajectories for 145 μm Al. (Black squares are nominal design)



We predict to be near optimum 33% peak cone fraction and outer cone pointing to minimize P2, P4 in 575-scale hohlraum (case-capsule ratio = 2.6)

Surface non-concentricity is modeled as P1 thickness variation

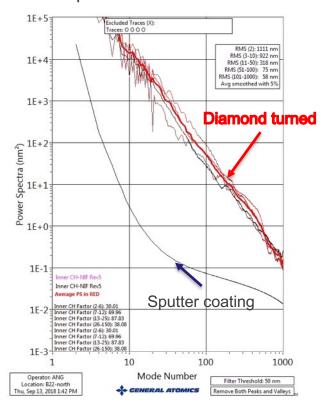




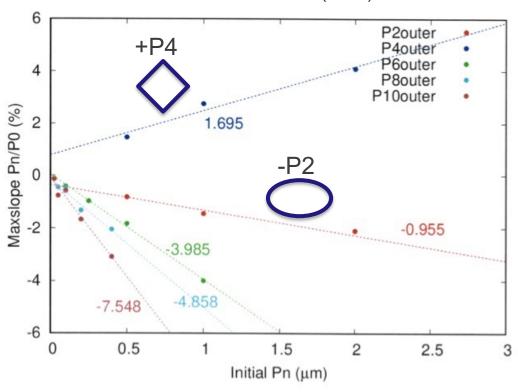
Full hohlraum radiation smoothing turned on

Machined surface spectra motivates the need for outer and inner surface mode sensitivity studies

Diamond turned Al shell outer surface spectra show higher amplitudes than sputter coated shells



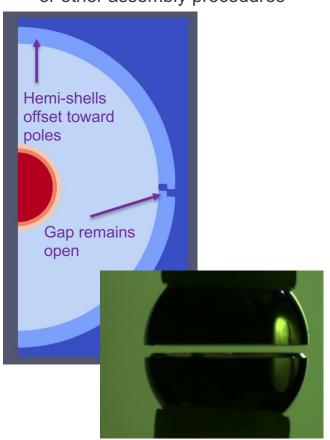
Increasing mode number leads to higher growth factors for outer surface (even) modes 2-10



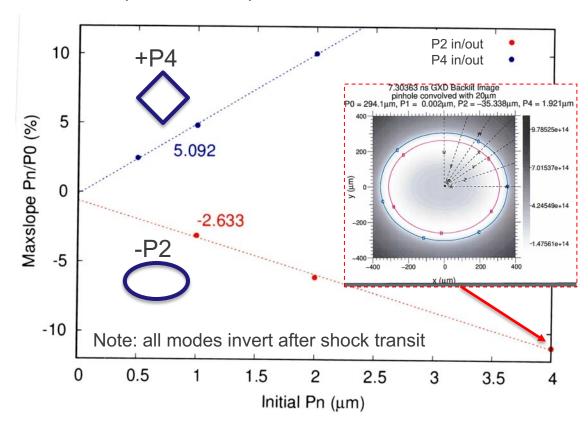
- Higher low-mode power relative to sputter coating comes from non-closure of joint gap (see next slide)
- Recent fabrication improvements have substantially reduced gap closure along with low modes (see backup slides 23 and 24)

Non-closure of equatorial gap is a dominant source of low-modes in surface spectra

Bulk ablator shape non-uniformities may arise during assembly due to joint misfits or other assembly procedures



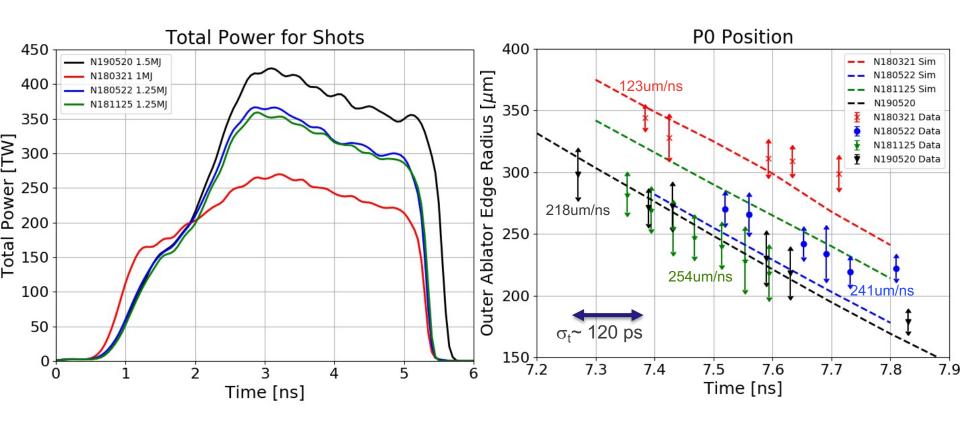
Predicted sensitivity to bulk ablator shape modes when same perturbation is placed on both inner and outer surface



Postshot modeling of experimental data

Simulated trajectories are within 0.15 ns of measurements with discrepancies possibly due to capsule fabrication*

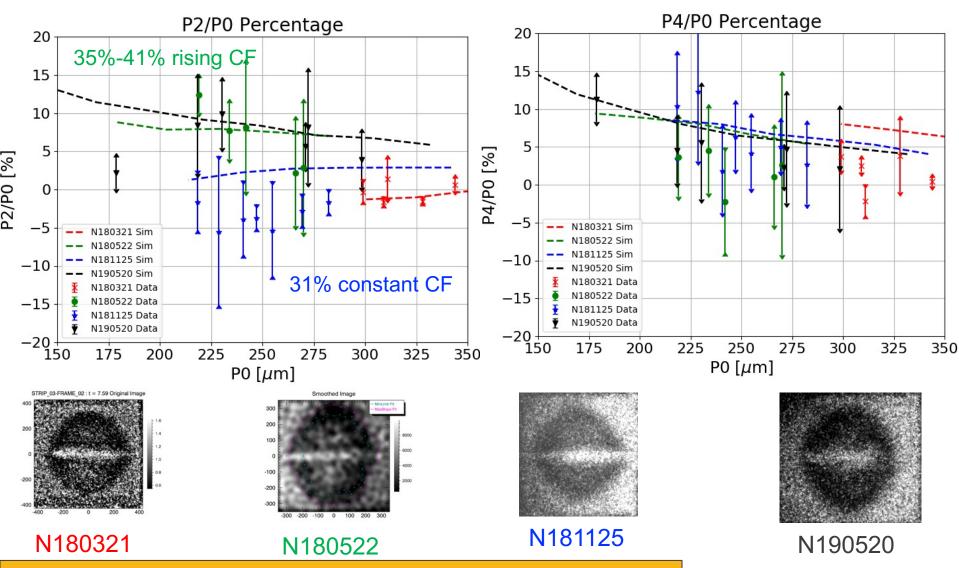
*Non-closure of joint gap



Backscatter on each shot has been <2% (see backup slides)



Simulated shape is generally in line with data, and changes in cone fraction predict the direction of the P2 change



 2DconA ablators used sub-scale thickness and had non-zero gap opening (see backup metrology slides 19-22)



Conclusions and next steps

Sensitivity studies of identified asymmetry sources

- Inward pointing of outer cones by 300 μm increases P4/P0 by 2%
- 4% change in P2/P0 observed for cone fraction change between 30-36%
- ~1 μm P1 thickness variation leads to ~3% P1/P0 at collision time
- Outer and inner surface modes show increasing growth rate up to imposed P10

Quantification of control

- Measured P2 shift due to designed cone fraction change was in qualitative agreement with HYDRA postshot simulations
- Need to confirm that lack of quantitative agreement with N181125 is due to capsule fabrication artifacts
- Better control currently limited by ablator fabrication
 - Equatorial joint gap closure to < 1 micron recently demonstrated
- Continue asymmetry source assessment of point design double shell performance (L2 milestone in FY22)



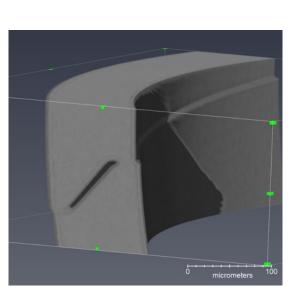
THANK YOU!

Metrology for N180321-003

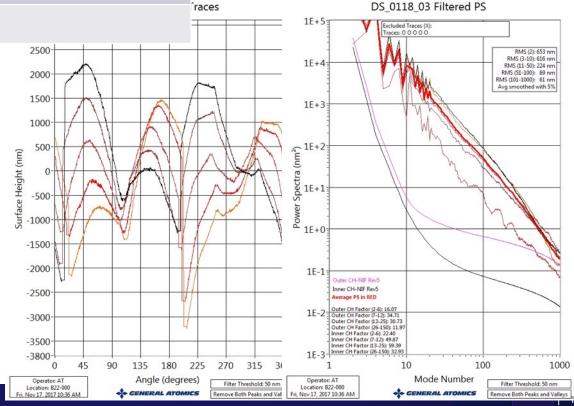
Dimension	measurement
Ablator thickness	106 micron
Joint gap	4-6 micron
Joint offset/step	?
Surface concentricity	TOP: ??? BOT: ???
Hohlraum length	

Compare top to bottom

Compare outer to inner



LEH diameter

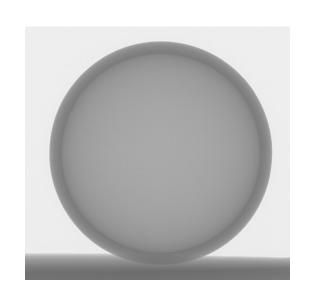


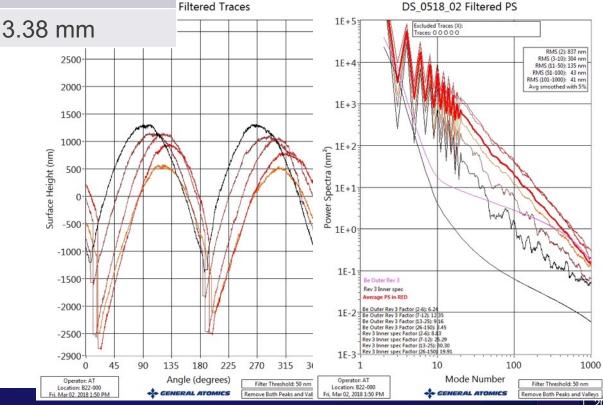
Metrology for N180522-002

Dimension	measurement
Ablator thickness	120 micron
Joint gap	>3 um
Joint offset/step	3 um in Y
Surface concentricity	TOP: 1 um in Y BOT: 1 um in X
Hohlraum length	10.16 mm
LEH diameter	3.38 mm

Compare top to bottom x or y

Compare outer to inner





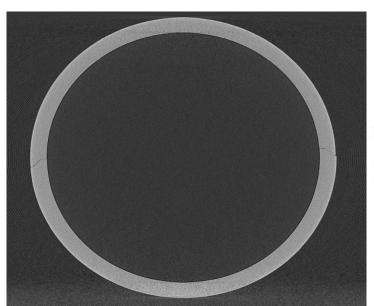
Metrology for N181125-003

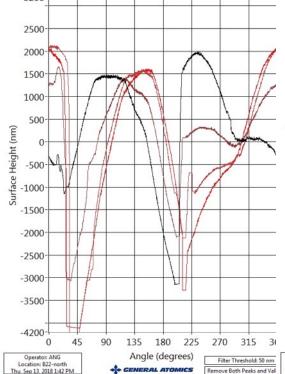
Started using Keyence IM

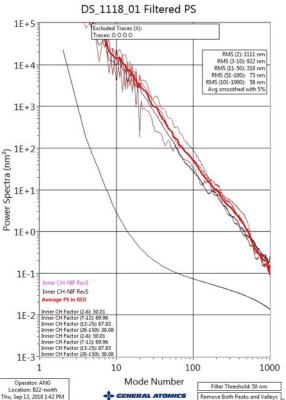
Dimension	Capsule 1	Capsule 2
Ablator thickness	120 micron	
Joint gap	5 micron	Below CT
Joint offset/step	3-6 um in X	4 micron in Y
Surface concentricity	TOP: 2 um vert BOT: 3 um horz	TOP: 0-1 um BOT: 3 um vert
Hohlraum length		
LEH diameter		

Compare top to bottom

Compare outer to inner







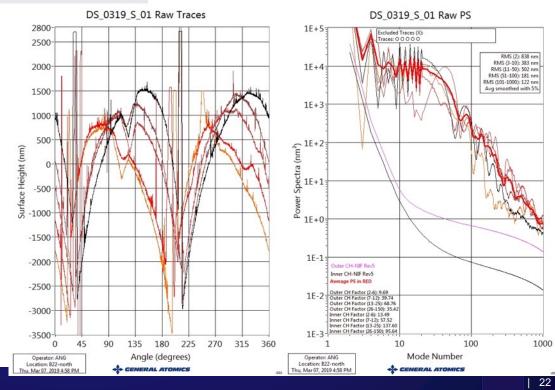
Metrology for N190520-002

motionegy for i	1100010
Dimension	Capsule 1
Ablator thickness	128 micron
Joint gap	7-10um
Joint offset/step	1-2 um in X
Surface concentricity	TOP: 2 um in X, Y BOT: 1 um in X
Hohlraum length	10.13 mm
LEH diameter	3.38 mm

Compare top to bottom x or y

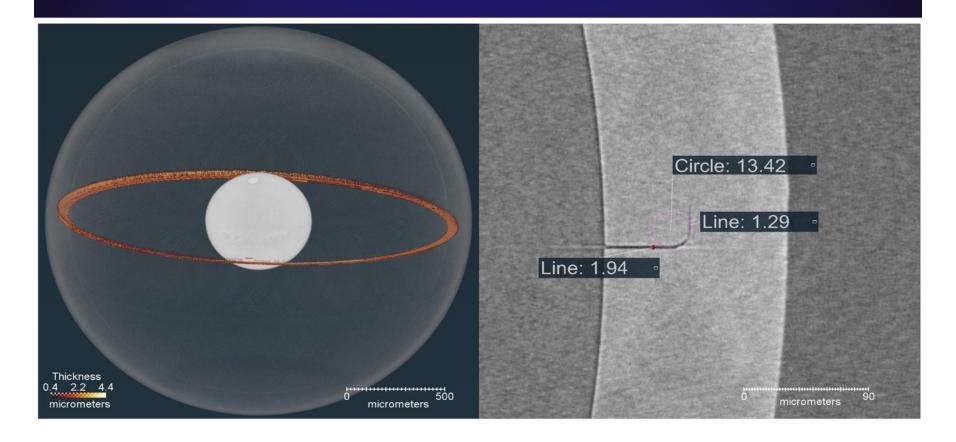
Compare outer to inner





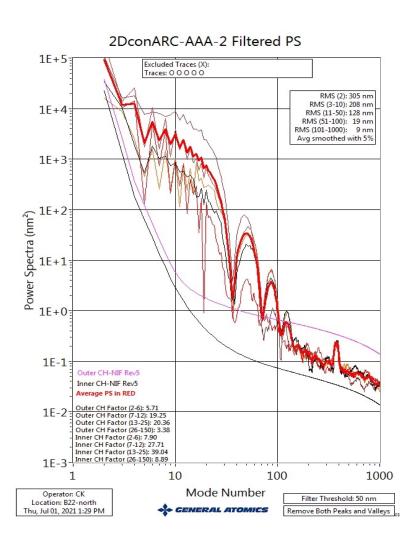
Improved fabrication is significantly reducing joint gap closure and ablator surface modes

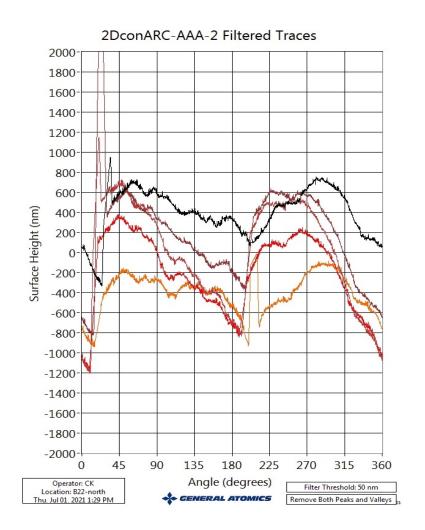
AAA-2 Joint thickness





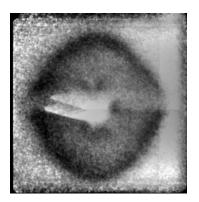
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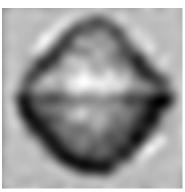




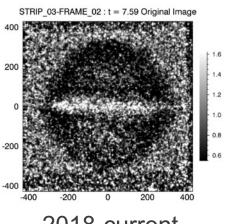


 Note N180321-003 was first shot moving to reduced P4 by shifting outer cone pointing, increasing hohlraum length, and reducing LEH size. Perhaps is useful to show N170322-001 image for comparison



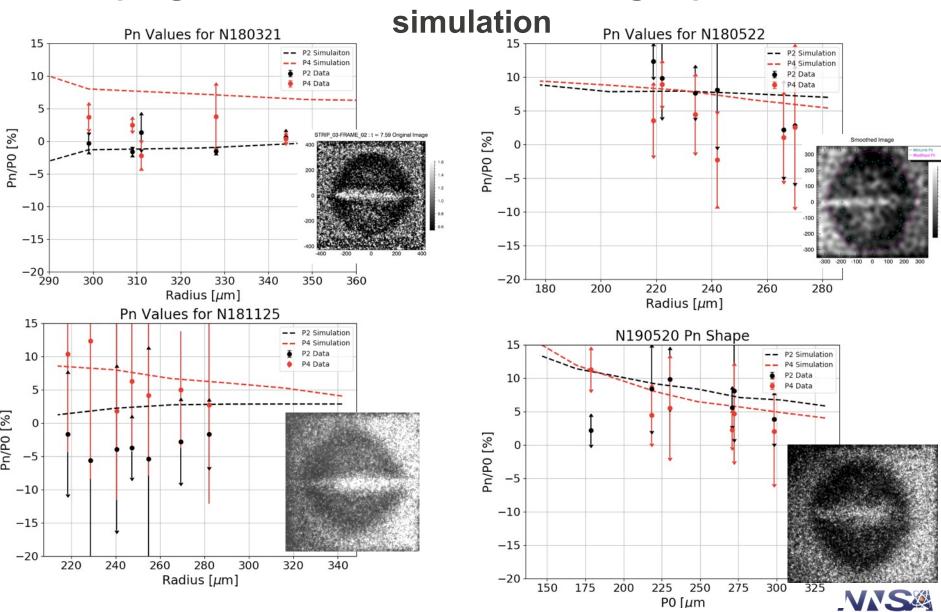


2017



2018-current

Shape values for each experiment show that there is still progress to be made in reconciling experiment and



The root mean square deviation (RMSD) gives a quantitative measure of how much experiment and simulation differ

- The RMSD is calculated by comparing the difference between experimental and simulated data points using the formula $RMSD = \sqrt{\frac{\sum_{i=1}^{N}(x_i \widehat{x_i})^2}{N}}$
- x_i is the experimental value, \hat{x}_i is the simulated value, and N is the number of experimental data points.
- Here predictability is defined as the RMSD being less than the average experimental error for a given measurement.

Shot	P0 RMSD [µm]	P0 Average Error [µm]	P2 RMSD [μm]	P2 Average Error [µm]	P4 RMSD [μm]	P4 Average Error [µm]
N180321	17.67	11.71	4.68	4.08	19.70	6.53
N180522	25.08	13.36	8.94	15.0	13.80	18.16
N181125	48.90	17.95	17.20	10.86	7.54	13.60
N190520	9.82	15.62	7.79	10.81	6.57	13.59



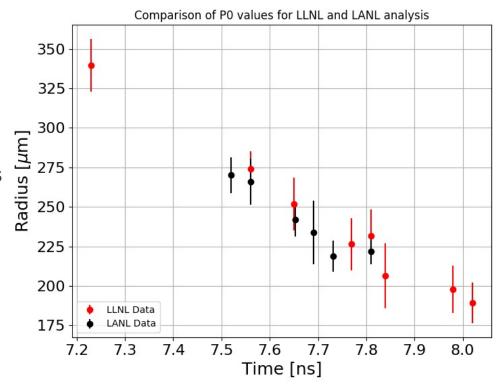
Uncertainty estimation in shape analysis (Shahab Khan, LLNL)

Statistical

 Variations of the amplitudes found from decomposition of each iimage within a filter

Systematic

- Quadrature sum of correlation, subtraction, and smoothing errors
- Correlation: small translations of the image comparing resulting shape metrics
- Subtraction: varying size of ellipse that defines background region
- Smoothing: increase/decrease levels of smoothing; using gaussian kernels





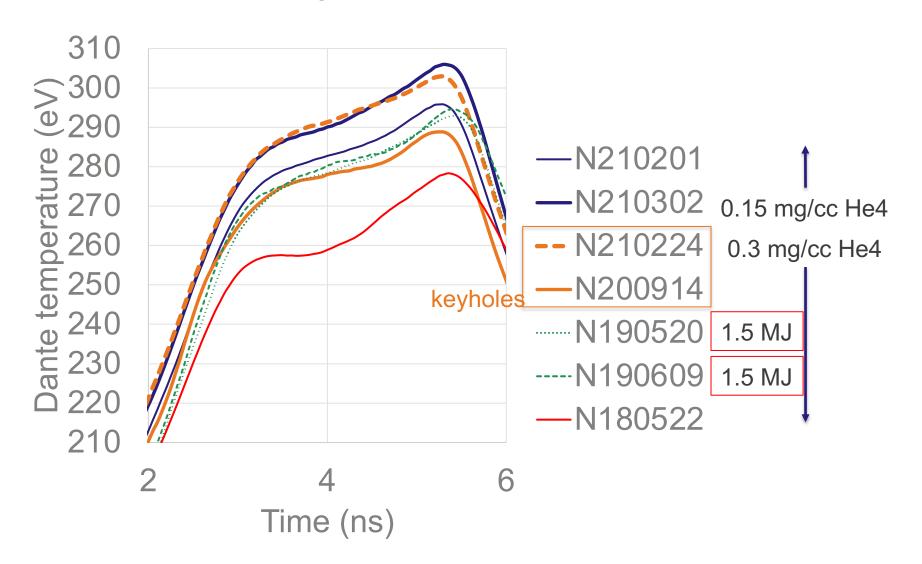
Backscatter results

11100120 001	Be capsule	Э	N160313-002	Be capsul	е	N170222-003	capsule		N170322-001	capsule	
Cone	Quad Estimate (kJ)	Cone Estimate (kJ)	Cone	Quad Estimate (kJ)	Cone Estimate (kJ)	Cone	Quad Estimate (kJ)	Cone Estimate (kJ)	Cone	Quad Estimate (kJ)	Cone Estimate (kJ)
23 deg. SRS		0.4	23 deg. SRS	0.03	0.24	23 deg. SRS	0.01	0.11	23 deg. SRS	0.02	0.12
23 deg. SBS		0	23 deg. SBS	0.54	4.29	23 deg. SBS	0.16	1.25	23 deg. SBS	0.15	1.21
30 deg. SRS		8.82E-03	30 deg. SRS	0.03	0.25	30 deg. SRS	0.03	0.27	30 deg. SRS	0.02	0.13
30 deg SBS		0.19	30 deg SBS	0.54	4.29	30 deg SBS	0.16	1.25	30 deg SBS	0.15	1.21
50 deg. SRS		0.01	50 deg. SRS	8.76E-03	0.14	50 deg. SRS	8.16E-03	0.13	50 deg. SRS	8.14E-03	0.13
50 deg. SBS		0.17	50 deg. SBS	0.06	1.02	50 deg. SBS	0.08	1.28	50 deg. SBS	0.07	1.16
44 deg. SRS		0.01	44 deg. SRS	8.76E-03	0.14	44 deg. SRS	8.16E-03	0.13	44 deg. SRS	8.14E-03	0.13
44 deg. SBS		0.17	44 deg. SBS	0.01	0.22	44 deg. SBS	0.02	0.28	44 deg. SBS	0.02	0.26
Total Backscatter (kJ)		0.97	Total Backscatter (kJ)		10.6	Total Backscatter (kJ)		4.69	Total Backscatter (kJ)		4.34
Laser Energy (kJ)		1021.86	Laser Energy (kJ)		994.43	Laser Energy (kJ)		1015.83	Laser Energy (kJ)		1010.27
Coupling		99.9	Coupling		98.93	Coupling		99.54	Coupling		99.57
N171016-001	Al capsule		N180321-003	Al capsule		N180731-002	Al capsule		N180918-001	Al capsule	
	0 1	Cone		Quad	Cone		Quad Estimate	Cone	0	Quad	Cone
Cone	Quad Estimate (kJ)		Cone	Estimate (kJ)	(kJ)	Cone	(kJ)	(kJ)	Cone	Estimate (kJ)	(kJ)
	Estimate	Estimate	Cone 23 deg. SRS			Cone 23 deg. SRS		(kJ)	23 deg. SRS		(kJ)
23 deg. SRS	Estimate (kJ)	Estimate (kJ)		(kJ) 0.04	(kJ)		(kJ) 0.04	(kJ) 0.28		(kJ)	(kJ) 0.2
23 deg. SRS 23 deg. SBS	Estimate (kJ) 0.03	Estimate (kJ) 0.25	23 deg. SRS	(kJ) 0.04	(kJ) 0.31	23 deg. SRS	(kJ) 0.04	(kJ) 0.28 0.07	23 deg. SRS	(kJ) 0.03	(kJ) 0.24 0.21
23 deg. SRS 23 deg. SBS 30 deg. SRS	Estimate (kJ) 0.03 0.07	Estimate (kJ) 0.25 0.53	23 deg. SRS 23 deg. SBS	(kJ) 0.04 5.74E-03	(kJ) 0.31 0.05	23 deg. SRS 23 deg. SBS	(kJ) 0.04 8.61E-03	(kJ) 0.28 0.07 0.27	23 deg. SRS 23 deg. SBS	(kJ) 0.03 0.03	(kJ) 0.24 0.20
Cone 23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS	Estimate (kJ) 0.03 0.07 0.04 0.07	Estimate (kJ) 0.25 0.53 0.31	23 deg. SRS 23 deg. SBS 30 deg. SRS	(kJ) 0.04 5.74E-03 0.05 0.07	(kJ) 0.31 0.05 0.41	23 deg. SRS 23 deg. SBS 30 deg. SRS	(kJ) 0.04 8.61E-03 0.03 0.07	(kJ) 0.28 0.07 0.27 0.56	23 deg. SRS 23 deg. SBS 30 deg. SRS	(kJ) 0.03 0.03 0.04 0.06	(kJ) 0.24 0.3 0.4
23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS	Estimate (kJ) 0.03 0.07 0.04 0.07	Estimate (kJ) 0.25 0.53 0.31 0.53	23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS	(kJ) 0.04 5.74E-03 0.05 0.07	(kJ) 0.31 0.05 0.41 0.53	23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS	(kJ) 0.04 8.61E-03 0.03 0.07	(kJ) 0.28 0.07 0.27 0.56 0.14	23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS	(kJ) 0.03 0.03 0.04 0.06	(kJ) 0.24 0.30 0.45 0.45
23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS	Estimate (kJ) 0.03 0.07 0.04 0.07 8.87E-03 0.98	Estimate (kJ) 0.25 0.53 0.31 0.53 0.14	23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS	(kJ) 0.04 5.74E-03 0.05 0.07 7.74E-03 0.81	(kJ) 0.31 0.05 0.41 0.53 0.12	23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS	(kJ) 0.04 8.61E-03 0.03 0.07 8.60E-03 0.84	(kJ) 0.28 0.07 0.27 0.56 0.14 13.38	23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS	(kJ) 0.03 0.03 0.04 0.06 8.21E-03	(kJ) 0.24 0.3 0.49 0.13
23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS 50 deg. SBS 44 deg. SRS	Estimate (kJ) 0.03 0.07 0.04 0.07 8.87E-03 0.98	Estimate (kJ) 0.25 0.53 0.31 0.53 0.14 15.62	23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS 50 deg. SBS	(kJ) 0.04 5.74E-03 0.05 0.07 7.74E-03 0.81	(kJ) 0.31 0.05 0.41 0.53 0.12 12.9	23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS 50 deg. SBS	(kJ) 0.04 8.61E-03 0.03 0.07 8.60E-03 0.84	(kJ) 0.28 0.07 0.27 0.56 0.14 13.38 0.14	23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS 50 deg. SBS	(kJ) 0.03 0.03 0.04 0.06 8.21E-03	(kJ) 0.24 0.3 0.49 0.13 16.33
23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS 50 deg. SBS	Estimate (kJ) 0.03 0.07 0.04 0.07 8.87E-03 0.98 8.87E-03	Estimate (kJ) 0.25 0.53 0.31 0.53 0.14 15.62 0.14	23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS 50 deg. SBS 44 deg. SRS	(kJ) 0.04 5.74E-03 0.05 0.07 7.74E-03 0.81 7.74E-03	(kJ) 0.31 0.05 0.41 0.53 0.12 12.9 0.12	23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS 50 deg. SBS 44 deg. SRS	(kJ) 0.04 8.61E-03 0.03 0.07 8.60E-03 0.84 8.60E-03	(kJ) 0.28 0.07 0.27 0.56 0.14 13.38 0.14	23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS 50 deg. SBS 44 deg. SRS	(kJ) 0.03 0.03 0.04 0.06 8.21E-03 1.02 8.21E-03	(kJ) 0.24 0.26 0.3 0.49 0.13 16.33 0.13
23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS 50 deg. SBS 44 deg. SRS 44 deg. SBS Total Backscatter	Estimate (kJ) 0.03 0.07 0.04 0.07 8.87E-03 0.98 8.87E-03	Estimate (kJ) 0.25 0.53 0.31 0.53 0.14 15.62 0.14 3.44	23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS 50 deg. SRS 44 deg. SRS 44 deg. SBS Total Backscatter	(kJ) 0.04 5.74E-03 0.05 0.07 7.74E-03 0.81 7.74E-03	(kJ) 0.31 0.05 0.41 0.53 0.12 12.9 0.12 2.84	23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS 50 deg. SRS 44 deg. SRS 44 deg. SBS Total Backscatter	(kJ) 0.04 8.61E-03 0.03 0.07 8.60E-03 0.84 8.60E-03	(kJ) 0.28 0.07 0.27 0.56 0.14 13.38 0.14 2.94	23 deg. SRS 23 deg. SBS 30 deg. SRS 30 deg SBS 50 deg. SRS 50 deg. SRS 44 deg. SRS 44 deg. SBS Total Backscatter	(kJ) 0.03 0.03 0.04 0.06 8.21E-03 1.02 8.21E-03	(kJ) 0.24 0.3 0.49 0.13 16.33 0.13

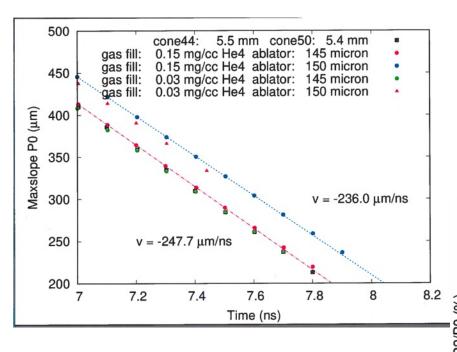
N180522 had 99% N190609 had 99% N181125 had 98%

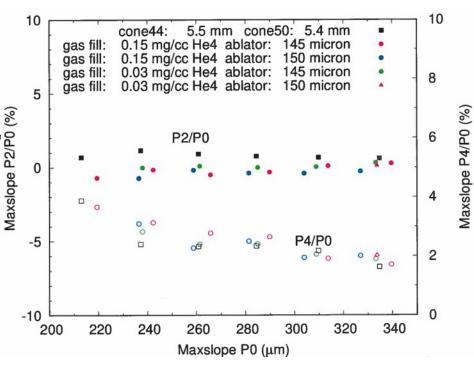


Better drive performance at 0.15 mg/cc fill or systematic change to Dante since FY19?

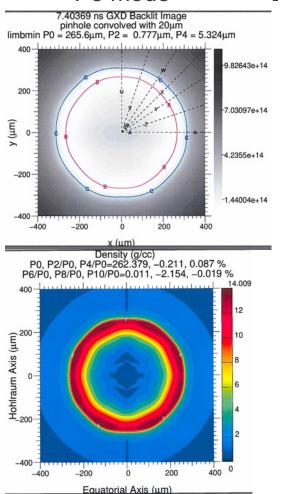


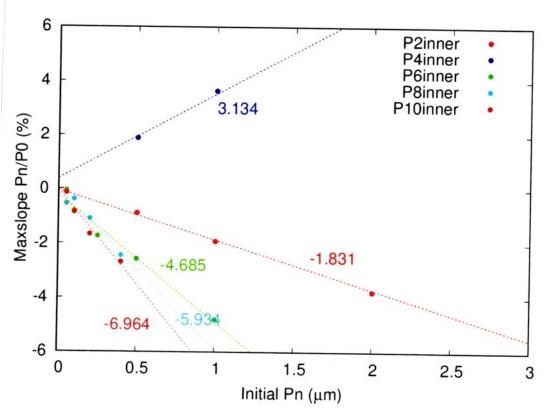
Sensitivity to hohlraum gas fill





HYDRA inner surface ablator P8 mode mode results

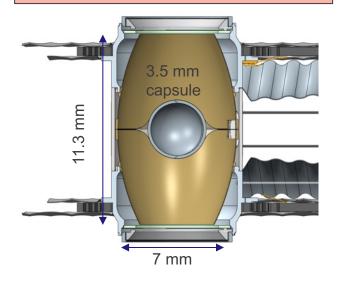




Inner surface modes grow moderately faster than outer surface modes

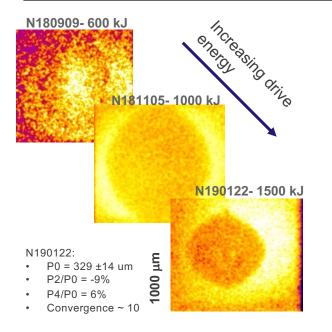
LLNL is exploring larger scale hohlraum platforms to significantly enhance energy coupling

Advanced hohlraums are expected to couple 3-4x more energy to capsule



RI: Y. Ping, V. Smalyuk (LLNL) Designer: P. Amendt (LLNL)

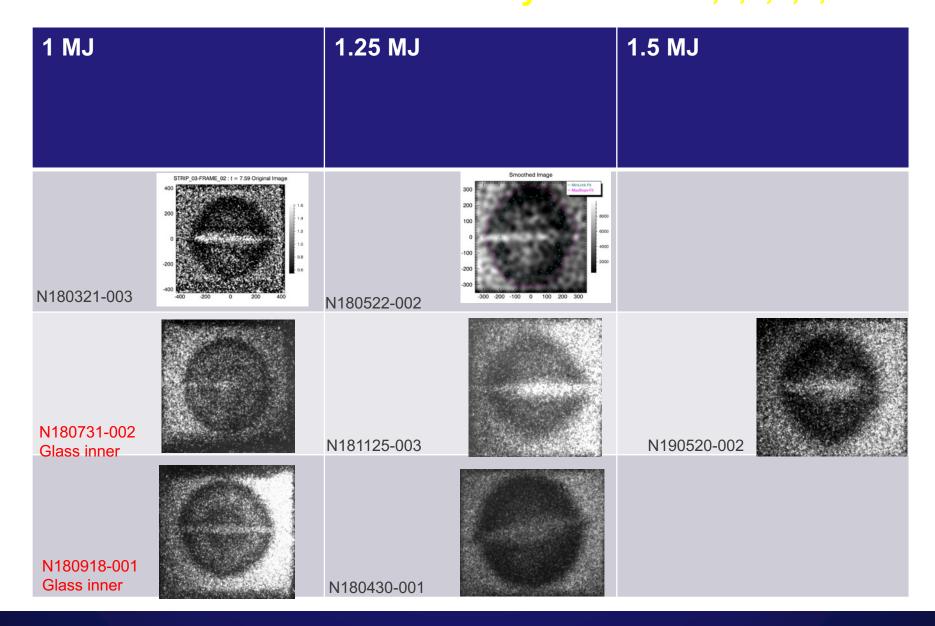
In-flight radiography of large outer shell



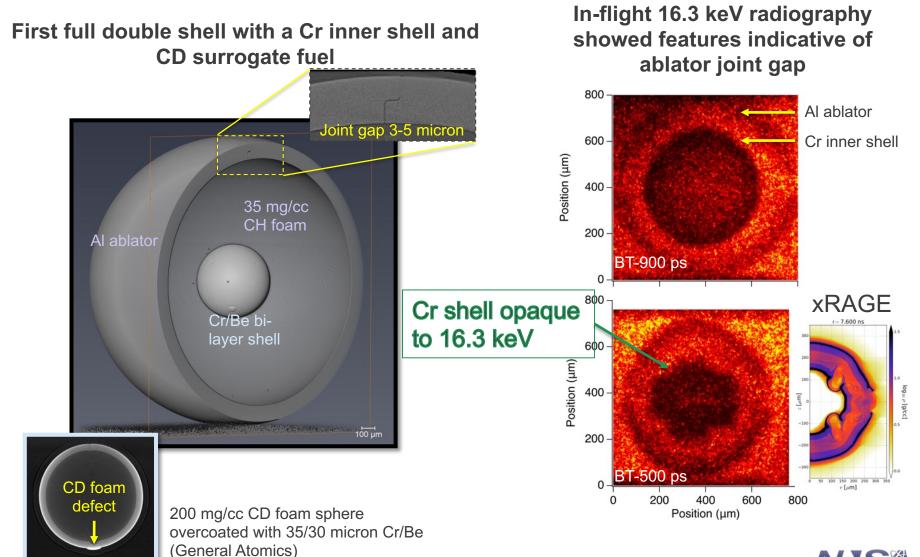
*Y. Ping et al., Nature Physics (2018)



Radiography data summary



March 2021 double shell 2DconA showed evidence of a joint feature dominating inner shell shape



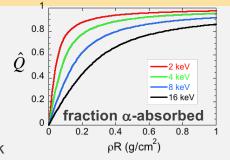
High-Z shells offer new opportunities to assess power balance in a confined, burning plasma

*Montgomery, Daughton et al., Phys. Plasmas 25, 092706 (2018)

Fusion heating rate must exceed expansion losses

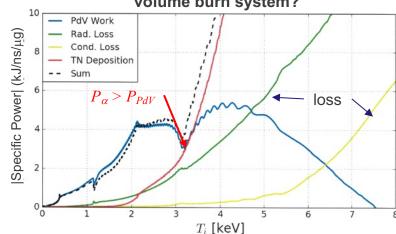
$$T_{keV} > \frac{4}{\left(\rho R_* f_{tamp} \ \hat{Q}\right)^{0.4}}$$

- Ensures burn begins before peak compression
- 'Robust' to implosion asymmetries and pusher/fuel mix
- Does not include radiation losses...



ρR (g/cm²)	T (keV)
0.25	> 4.6
0.35	> 3.9
0.60	> 3.1

How important are radiation losses in a volume burn system?

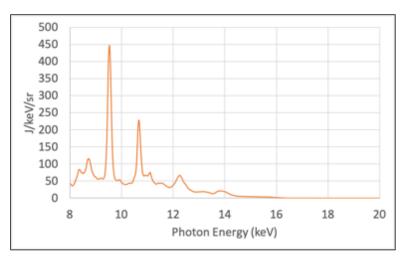


Mass-averaged fuel temperature



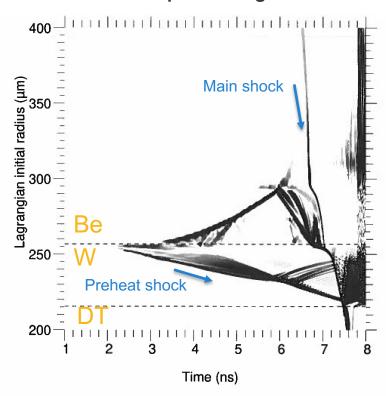
FY20/21 keyhole experiments used to constrain shock and preheat as independent sources of asymmetry for high-Z inner shell

Au L-shell spectrum measured through LEH on keyhole shot N200914-001



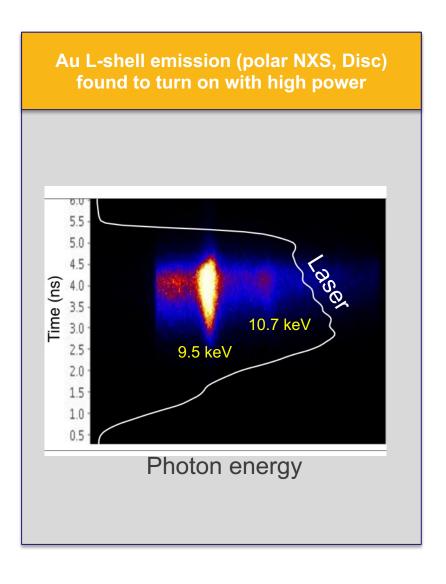
NXS analysis, C. Krauland (GA)

HYDRA shock trajectories in double shell point design



- Preheat (Au L-shell) and main shock set inner shell adiabat
- Accurate Au L-shell modeling requires non-local thermal conduction and nLTE DCA opacities

February 2021 keyhole made first measurement of preheat asymmetry in a double shell



Raw line VISAR data showing W inner surface motion. Used 20 micron W and 20 micron Be shell

